## Title 14-derenantics and space

Chapter I-Federal Aviation Agency

[Docket Nos. 8810, 7046; Amdt. No. 87-0]
PART 37—TECHNICAL STANDARD
ORDER AUTHORIZATIONS

Crewmember Demand Oxygen Masks, TSO—C78; Oxygen Regulators, Demand, TSO—C89

The purpose of this amendment is to add new Technical Standard Orders (TSO's) for crewmember demand oxygen masks and demand oxygen regulators to Part 37 of the Federal Aviation Regulations. These TSO's contain the minimum performance standards that such masks and regulators must meet in order for manufacturers to identify them with the applicable TSO markings.

The standards for crewmember demand oxygen masks were published as a notice of proposed rule making (30 F.R. 9547, July 30, 1965) and circulated as Notice 65-18 dated July 26, 1965. The standards for demand oxygen regulators were published as a notice of proposed rule making (30 F.R. 15294, Dec. 10, 1965) and circulated as Notice 65-36 dated December 3, 1965. Because of the similarities and technically related aspects of the two standards, they are being simultaneously promulgated in this

amendment to Part 37.

Numerous somments were received in response to Notices 65-18 and 65-36. The more pertinent of these comments together with the changes in the proposals resulting therefrom are discussed in detail hereinafter.

The parenthetical reference "air carrier or transport category aircraft" and the phrase "to be used on air carrier or transport category civil aircraft" have been deleted from the section catchlines, the titles of the Standards, and the applicability statements of the final regulations. Such statements have cresome confusion and they serve no useful purpose insofar as the TSO's are concerned. A TSO contains those standards a manufacturer must meet in order to identify his equipment with the appli-cable TSO marking. A manufacturer desiring to use the applicable TSO marking must meet the prescribed Standard regardless of the type of operation or the type of aircraft in which the equipment might be used. Thus, the performance standards set forth in the TSO's are mandatory only for equipment manufactures who wish to obtain TSO authorization covering their equipment and are not directed to persons who install or use such equipment in aircraft.

Crewmember demand oxygen masks. Concerning the status of presently approved and installed masks after the effective date of the TSO, two commentators recommended inclusion of a state-

(As published in the Federal Register 732 P.R. 1257 on January 7, 1967)

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ment that presently approved masks can continue to be manufactured and installed and that the TSO relate m only to new design masks. As previously stated, this TSO contains minimum performance standards that oxygen masks must meet in order for the manufacturer to identify it with the applicable TSO mark. The TSO is not directed to persons who install or use this equipment in aircraft. From an operational stand-point, the Technical Standard Order system merely provides one means by which equipment is approved. Unless the operating rules require equipment to be TBO approved, an operator may use any approved equipment. From the standpoint of the identification of a piece of equipment as being TBO approved, the applicability statement of the TSO clearly states that it is only "new models" of oxygen masks that must meet the new Standard in order to be identified as being manufactured under a TBO authorization. However, consistent with other TBO's the Agency considers it appropriate to include a provision specifically indicating that presently approved masks may continue to be manufactured under the provisions of the original ADDTOVAL.

One of the preceding commentators also suggested specifying the extent to which a TBO-approved mask can be modified before it is considered a new model requiring TSO requalification and the extent to which a non-TSO mask can be modified before it must be qualified under the TBO. The Agency does not believe the proposal need be change in this regard since design changes in articles manufactured under a TSO authorization are objectively covered in § 37.11 of Subpart A of Part 37, and design changes to non-TBO items are outside the scope of Part 37.

Paragraph 2.2 of the TSO allows protective goggles to be included as part of the mask. One recommendation would add vision restriction limits for full face (smoke protection) masks and another would require marks not incorporating integral goggles to be designed for use with standard full-eye protection gog-gles. While the intent of the TBO is to permit the oxygen mask to serve as a smoke mask where eye protection is provided, the detailed standards relate only to oxygen masks. The recommenda-tions, therefore, are beyond the scope of the TSO and must be rejected.

One manufacturer recommended that paragraph 2.4 quantitatively define the amount of expiratory gases permitted to accumulate within the facepiece cham-The actual facepiece chamber volume that constitutes a hazard in any giyen mask, however, depends on a number of interrelated factors i.e., maximum approved altitude, inlet valve design, etc. Since these variables make regulatory quantification impracticable, the proposal has not been changed as suggested.

Four commentators took exception to proposed paragraph 2.5 which would have required that expiratory gases not impinge on the inhalation port or vaive. masks the inhalation valves receive impingement of expiratory gases which in the case of coaxial valves, actually assists in opening the exhalation po Since inhalation valves are not subje to the collection of moisture and frost, as are exhalation valves, the Agency agrees that the requirement is unneces-sary and proposed section 3.5 has been deleted.

Proposed paragraph 2.6 stated the basic requirement that most design must prevent frost interference with exhalation valve functioning. One commentator suggested deletion of the exemption to the basic requirement that w frost removal from the exhalation valve by external manipulation if it can be shown that such removal can be seen plished without removing the mask. Since it is unlikely that frost buildup. even if encountered, would need frequent removal by external manipulation, the Agency believes that this exception is agency Seneves that this exception is appropriate. Proposed paragraph 3.6 (now paragraph 3.5) is, therefore, adopted without change.

Comments on proposed paragraph 3.8 noted that the hose disconnect warning

device requirement appears to be more a system specification than a mask speci-Scation and recommended a higher flow restriction percentage to provide a bet-ter warning. Actually, the restriction device will be installed in the mask supply line and, therefore, is a part of the k assembly. The 25 percent m mum restriction value was determined by the Civil Aeromedical Research Institute. Oklahoma City, which considered, inter alia, that too high a restriction introduces the danger of lung collapse. paragraph (now 2.7) is being retained as

With reference to the quick-disconnect coupling set forth in paragraph 3.1, one commentator recommended a reduction in the minimum symmetrical separation force to 10 pounds following the military specification, while another commentator suggested that the stated force should be the minimum regardless of the direction of application. The Agency agrees that the minimum separation force may be set at 10 pounds but does not believe t necessary to specify minimum non-ymmetrical separation forces since in those cases, a force applied along a non-symmetrical axis would probably be higher, not lower, than the symmetrical eparation force. Paragraph 3.1 has seen amended to reflect the 18-pound minimum force exerted along the axis of symmetry.

A number of comments were addressed to the leakage performance requirements of paragraph 3.3. As to a recommendation that the TSO specify outward leakage requirements for pressure demand masks, the Agency does not believe it necessary inasmuch as small outward leaks, while wasteful, do not impair proper operation of the mask and large leakage rates would be readily detectable and stopped by the wearer by adjusting the fit of the mask. Two recommendations to increase the 0.10 LPM STPD impinge on the inhalation port or valve. inward leakage rate must be rejected. They pointed out that in many present since this value already represents the

highest portion of the maximum total green leakage allocable to the most. Various recommendations that the neg-Various reco ative differential pressure range ever which the leakage rate is applicable be either increased or decreased were unsupported and the values as proposed

One commentator reco paragraph 3.3 include a test requires that the mask be sealed to the face or test plate and that the look test is the hose-to-regulator connector. intent of the requirement, however, is that the leakage rate specified for the given range of differential pressures he applicable to the mask as normally wern on the face (makeding the effects of mask on the face (meluting the effects of mask fit to the face) or to the mask positioned on a mitable equivalent test stand and not to a mask sealed against peripheral leakage. Paragraph 3.3(a) has, therefore, been amended to make it clear that the leakage standard pertains to the mask as normally used. This change makes it unnecessary to include specific mention of the beaute-peripheral to the peripheral to ation of the home-to-regulator

A number of comments recommended changes to the numerical values contained in the tables in paragraphs 3.4 (a) and (b) allegedly to reduce the fatiguing effect due to flow resistance. However, effect due to flow resistance. However the agency's evaluation of these reco mendations indicates that in as stances there is no fatiguing effect to be relieved while in others, a change would reserves while in others, a change would actually increase breathing resistance. At the maximum flow rate, fatigue is not a factor because of the short time duration involved. In still other cases, the suggested changes are equivalent in effect to the values given in the table. Therefore, the proposal has not been changed as suggested. However, the Agency does find merit in the suggestions that the oxygen supply tube referenced in paragraph 3.4(a) should include the oxygen supply connector and that, since expiratory gases do not flow through the supply tube, the reference to the oxygen supply tube in paragraph 3.4(b) should be deleted. Paragraphs 3.4 (a) and (b) are changed accordingly.

Proposed paragraph (c) of section 3.4 provides that the mask must not suffer samage at gas flows up to and including Subsequent review of this 120 T.PM proposal in light of comments received reveals that since 100 LPM is the maximum inhalation flow rate that would occur after substantial exercise, there is no need to test for damage at 120 LPM Paragraph 3.4(c) has, therefore, been deleted

In response to comments concerning ed to clarify the proposed paragraph 3.5, the Agency has rewritten the soure-demand exhalation valve performance standard to remove any ambi-guity concerning the facepiece pressure and supply tube pressure requirements for valve opening. Pointing out that a mask in use will

not be subjected to the frequency, acceleration, and amplitude enumerated in proposed paragraph 3.5(b), one sommentator concluded that the vibration standard applies to the stowed condition and recommended a change to require that the mask comply with paragraphs 3.3 through 3.5 after being subjected to the vibrations stated in paragraph 3.6(b). Upon further review, the Agency agrees that such a test does not represent a minimum requirement, and, noting that military specifications do not require vibration tests, has deleted the requirements proposed in paragraphs 3.6 (b) and (c).

The low temperature storage and test temperatures proposed in paragraphs 3.8 and 3.9 were stated to be unreasonably low by two persons who proposed higher temperatures. The Agency agrees that storage at -67° P. as required in paragraph 3.5 is unrealistic and the to ature has been raised to 0° F. Likewise, for the low temperature test delay set forth in paragraph 3.9, 20° P. in place of -40° P. is considered adequate to insure proper operation. Both the storage temperature in paragraph 3.9(a) and the the storage test temperature in paragraph 3.9(b) are changed accordingly. A further suggestion that paragraph 3.9 be reworded to refer to "delay apparent to the user" rather than "apparent delay to the user" points up an ambiguity in that paragraph. Since the intent of the paragraph is to preclude any apparent delay. the words "to the user" are inappropriate and the paragraph has been revised accordingly.

Various comments were directed to the decompression requirements for masks not equipped with pressure relief valves as stated in proposed paragraph 3.10(a). One suggested that the high operating altitude of the supersonic transport might influence the depressurization pressure ranges. Another recommended inclusion of human "subjective" testing at the maximum approved altitude.

In connection with the foregoing, the maximum approved altitude criterion for masks is based on the maximum environmental (cabin) altitude rather than maximum aircraft operating altitude. Thus, for the supersonic trans-port where cabin altitudes in the event of decompression are expected to be no higher than 40,000 feet even though the airpiane may be operating at 70,000 to 80,000 feet, the mask described in this proposal will be satisfactory. The Agency does not believe that it is necessary to specify human subjective test-ing at the maximum altitude although it does agree that the tests should properly simulate conditions of use. have, accordingly, amended paragraph 3.10 to require decompression tests under conditions simulating those of the mask being worn by a crewmember.

The proposed 10-assemd decompression test time in paragraph 3.10(a) was geared to the large type airplanes. A related comment correctly points out that this time is unrealistic and unsafe for the small volume, high-performance airplanes which may undergo decompression in less than 3 seconds. One manufacturer stated that a 1-second, or even shorter, decompression time requirement would impose no additional design or manufacturing burden on mask suppliers. Therefore, to accom-

modate the wide variety of cabin volumes of high-altitude aircraft in which the mask may be used, the decompression test time requirement has been decrassed from 18 seconds to 1 second.

Noting that values for pressure relief valve operation are not valid unless revalve operation are not valid unless re-lated to minimum regulator requirements that have not yet been established by the Agency, one commentator contended that sure relief valve schedule given in proposed paragraph 3.18(b) was too low. Assuming a regulator pressure on the order of 18 inches H.O to be required at 45,000 feet, the spread between opening and maximum was declared to be too small as was the proposed maximum pressure on opening. The schedule was further considered unrealistic and imctical in that it required the pressure relief valve to regulate and to close at the same pressure, whereas the closing point must be slightly below the minimum regulating pressure.

In connection with the foregoing comments, the mask requirements have been made compatible with those of the requisions being promulgated simultaneously in this rule-making action. On this basis, the Agency agrees that the pressure achedule should be increased and paragraph 3.18(b) has been amended to require an opening pressure of 17" H.O. maximum pressure within 5 minutes 16" H.O. maximum differential pressure 36" H.O. and closing pressure 14" H.O. Interpreting the simulated breathing

Interpreting the simulated breathing schedule of paragraph 3.11 as requiring a total of only 25,000 cycles, one commentator recommended a tenfold increase in the number of cycles. Insofar as this comment indicates an ambiguity in the number of cycles required, we concur with the need for change. However, we do not agree that 250,000 cycles are necessary. The intent of the requirement is to assure adequate reliability rather than to establish minimum service life. Since the proposed schedule is additive as to the number of required cycles, the paragraph is amended to make clear that the total is \$5,000 cycles.

In response to another comment, the last sentence of paragraph 2.11 is amended to state a requirement for a constant time interval between respiratory cycles.

In addition to the requirement that the microphone not interfere with the mask, it was suggested that the requirements of paragraph 3.12 should state that the operation of the mask must not interfere with use of the microphone and that qualitative tests be included to assure compliance with both of these requirements. However, since mask-microphone compatibility is a system requirement rather than a mask performance requirement; the TBO is properly limited to performance requirements that will insure proper operation of the mask. Nor does the Agency believe that qualitative tests are necessary in this regard since compatibility will be checked during approval of the installation in an aircraft.

Several comments were directed to the quality control production tests, paragraph 4.1, which are simply an inward

leakage test. One commentator thought the tests insufficient to establish that each mask assembly had been assembled correctly and suggested that more stringent production tests be required. In this connection, however, demension of the inward leakage rate of each mask is considered adequate for prediction tests since the quality control procedures of the manufacturer are examined as a part of the TSO approved process prescribed in §§ 37.3 and 37.15 of the FARs. Two other commentators noted that the leakage determination is not required to be made on masks for different sized and shaped hass. The purpose of the leakage production test is, among other things, to check whether the mask's flexible seal is capable of making a low-leakage connection with a surface having a face-like shape. It is not intended to insure a low-leakage fit on each prospective user of the mask, or even to insure a low-leakage fit on a variety of face shapes. A single face-like shape could conceivably be used to test a full production run.

Speaking to the quality control random tests, paragraph 4.2, one commentator recommended that lot sizes be at least 1,000 and that the requirement to comply with paragraphs 3.8(b), 3.8(c), 3.7, and 3.9(b) be deleted in view of the cost of the tests. The proposal, however, does not place a low limit on the let size but rather leaves it to the selection of the applicant subject to approval of the Agency. Also, proposed paragraphs 3.8 (b) and (c) have been deleted as discussed before. To insure adequate testing of random samples, the Agency believes it necessary to retain the acceleration load test, paragraph 3.7 and the low temperature delay test at the low temperature, paragraph 3.9(b). Some of the objection to the latter may have been met by relaxation of the test temperature as previously discussed.

Comments received concerning proposed paragraph 5.0 contained various recommendations that the 40,000 feet maximum operating altitude for straight or diluter-demand masks be either increased or decreased. However, the use of straight and diluter-demand masks at altitudes up to 40,000 feet has been allowed under current airworthiness regulations for some years. On the is of their service record, the Agency sees no need to reduce the maximum operating altitude. On the other hand, the Agency does not have enough data to justify increasing the maximum altitude for straight or diluter-demand masks as quested and the information submitted with the recommendation for such an increase does not contain the nece tification. Therefore the provisions of paragraph 5.0 are adopted as proposed.

From the comments received concerning paragraph 8.6 it is apparent that the term "maximum operating altitude" as used in that paragraph has created some confusion since it may be interpreted as referring to aircraft operating altitude rather than the altitude of the environment in which the mask is being used (cabin altitude) as was intended. To make it clear that paragraph 8.8 of the

TSO is not an operating requirement, it has been amended by deleting the term "maximum operating altitude" and using instead the term "maximum environmental (cabin) altitude."

Oxygen regulators. In response to a recommendation for clarification, we have amended paragraphs 2(c), 2(d), 3.5, 4.3(a), 4.2(b), 4.3(a), 4.5(a), and 4.6(b) to refer to pressure breathing regulators instead of pressure regulators as originally proposed.

Since, as one commentator correctly points out, exygen regulators may be designed for shoulder, chest, or other type mounting, paragraph 3.1 has been amended to provide for mounting on a crewmembers clothing or safety harness in addition to mounting on a mask.

We agree with the suggestion that, for fire protection, regulators must have self-extinguishing characteristics, even though they may be constructed of plastic type materials. Paragraph 3.3 has, therefore, been amended by adding the requirement that regulators be at least flame resistant.

One commentator recommended that paragraph 3.3(a), applicable to all demand regulators, permit the filter to be placed at the oxygen inlet hose assembly as well as at the oxygen inlet port. The Agency agrees that this would allow the use of a larger and more reliable filter in the case of mask mounted regulators. The Agency also agrees with recommendations that the screen he not coarser than 200 mesh. Paragraph 3.3(a) has been amended to incorporate both recommendations.

Reading paragraph 3.3(b) as perpetuating a military requirement, one commentator recommended a change to permit only 100 meah screen in place of the 30 to 100 as proposed but gave no reason why the coarser meshes were thought to be unsatisfactory. The 30 to 100 meah range has been retained although the paragraph has been reworded to permit multiple agreen filters.

One manufacturer advised that regulators may be designed to provide undiluted oxygen by means other than closing the air inlet diluter port, for example, by sensing a certain supply tube pressure. The Agency agrees with a recommendation to broaden the requirement and has amended paragraph 3.4 to state objectively the requirement without specifying the design detail by which this is to be

Various suggestions were made to change the positive pressure of 11.0±1.0 inches H.O required by paragraph 3.5. At one end of the range it was recommended that a pressure of 3.5 inches H.O be considered in order to give a safety pressure capability to the regulator in case of fumes or smoke in the cockpit. The Agency, however, does not agree with this recommendation since (1) protective breathing safety pressure is not needed if the mask fit is proper and, (2) protective breathing equipment, when provided, may utilize a separate regulator and the normal regulator might not be used during smoke or fume emergencies. While nothing in the Standard would preclude a manufacturar from including,

as an added feature, a "safety pressure" feature, it should not be a minimum safety requirement. Other commentators, while agreeing with the 11-inch pressure base, recommended varying values in the permissible variation. The Agency agrees that the range of leakage check pressure can be extended and has accordingly amended the requirement to specify 11.0 ± 3.0 inches H.O.

One commentator recommended that mask-mounted regulators be excluded from the flow indicator requirement of paragraph 3.5 and further that "cylinder oxygen" for which a flow indicator is required be changed by deleting the word "cylinder." Another commentator expressed betief that flow indication is required only for dilution type regulators since a crewmember will know by the increased section when a nondilution type regulator is not flowing oxygen. The Agency agrees with these recommendations and they have been incorporated into paragraph 3.5.

Several objections were made to the £2 inches of water outlet suction pressure required for the 100 LPM flow as stated in paragraph 4.1(a). Bligher outlet pressures, as generally recommended, would make it easier to achieve the specified flows but would require a greater breathing effort on the part of the using crewmember. The Asency agrees with one commentator that the pressure for the 100 LPM flow may be increased to 1.0 inches of water since the increased breathing effort would comment for only short periods of time during heavy breathing. However, an increase to 1.5 inches of water at all flows, as suggested by another, would require added breathing effort for long periods even during light or moderate breathing rates.

The Agency rejects a recommendation that paragraph 4.2 specify dynamic testing rather than static (constant flow) testing since experience has shown that regulators which meet constant flow requirements have been satisfactory under varying flow conditions. Likewise the Agency does not agree with a suggestion that the diluter-demand pressure column be deleted from the table in paragraph 4.2 (a) and that the diluter-demand column show the minimum for both diluter demand and diluter-demand pressure regulators insamuch as the oxygen mixture requirements are different for the two types.

A number of comments addressed the numerical table proposed in paragraph 4.2(a). One recommendation would have stopped altitude listing at 38,000 on the ground that there is no dilution above that altitude and dilution tables are not normally shown above 35,000. However, as presented, the table indicates the 40,000 feet environmental altitude limit of the diluter demand and the 45,000 feet limit of the diluter-demand pressure regulators and will therefore be retained. In this connection, the Agency does agree the table presented an ambiguity in showing a zero value as the percentage of cylinder oxygen for diluter demand at 45,000 feet when, in fact, the percentage of cylinder oxygen is not applicable at that altitude.

The Agency must reject a suggestion that the 91 percent shown in the paragraph 4.3(a) table for 25,000 he raised to 95 percent. While such a change would be consistent with existing military specifications, 91 percent provides the minimum traches oxygen partial presents required for physiological success, 24 manufacturer, of course, may provide in excess of 91 percent if he so elects. However, we do agree with another resemmendation that all values of 95 percent minimum percent expens in puragraphs 4.2 (a) and (b) be increased to 95 percent. This will provide a 3-percent allowance for system deficiencies such as mast lookage where the applicable airworthiness standards (a., PAR § 35.1443 (b)) require 95 percent expensions pressure altitudes above 25,000 feet.

As two commentators pointed out, flow rates at altitudes other than sea level, to

As two commentators pointed out, flow rates at altitudes other than sea level, to be meaningful, must be stated for conditions of ambient temperature and pressure. Therefore, paragraphs 4.3(a), 4.3, 4.4, 4.8 and 4.9 are amended to show ATPD in place of STPD.

Many comments were submitted with reference to the paragraph 4.3(a) table. The Agency does not agree that a minimum positive outlet pressure of 3.5 metes of water is required at 40,000 feet, since an adequate level of oxygen saturation will be maintained in the bleed when breathing nonpressurized oxygen at that altitude. For the same reason we do not believe that any positive safety pressure need be maintained at altitudes between 30,000 and 40,000 feet to prevent mask inhoard leakage. Moreover, the Agency does not agree with other recommendations that the minimum allowable positive outlet pressure be increased since the values proposed will provide adequate oxygen in the bloodstream. However, we agree that pressure tolerances may be widened at all specified altitudes and the table has been amended accordingly.

The Agency does not agree that the basic 20 LPM flow rate specified in paragraphs 4.3(a), 4.3(b), and 4.3(c) should be reduced insamuch as this value represents a normal breathing rate. Similarly, a recommendation that the range of flow rates in paragraph 4.3(c) be changed to 0.10–10 LPM was not supported by any justification.

Pointing out that there are other acceptable methods of measuring leakage rate, two commentators recommended deletion of the last sentence of paragraph 4.4(d) that proposed to determine leakage on the hasis of a decrease in pressure during a 3-minute period. The Agency agrees and has deleted the sentence. Also the ambiguous phrase "oxygen supply port" as proposed in paragraphs 4.4 (c) and (d) has been clarified to read "regulator outlet port."

In the proposed paragraphs 4.5 (a) and (b), we agree that the negative pressure stated in terms of inches of mercury should be stated in inches of water. Also, for the tests specified in the same paragraphs, it is necessary to darify that the regulator inlet port, as well as the diluter valve, be closed. Paragraphs 4.5

(as atid cb) have been amended to in-corporate these changes.

Assdiscussed proviously linethic presini-

ble in connection with TSO\_E73, Crewble in connection with TSE-ETB, Crew-brember demand oxygen masks, an allow-since of 10 seconds is not representable of the decompression interval that can oc-curinternal volume directate having high altitude canabilities. Pollowing a recom-time allowance, the Agency has deter mined, from the information spatialie, that imposition of a one-second decompression requirement will impose n o added design or manufacturing burden added design of manufactuding burden on the producers of regulators. In the interest of unitely, pangraphed 46(a) and (b) are amended to diseptate teached decompression expallities on all regulators. The Agency agrees with one configurations that perfeithance compliance at 160° F.

that performance compliance at 160° F. is unrecallific and has celluced that themperature to 130° F. In paragraph 4.7(c). In like vela, two commentations said the -480° F. proposed la paragraph 4.7(d) was too low and recommended it be set at +20°. We carge at that in the event of decompression, it would be unrealistic for the cabir its cremain at -- (6° Ro long enough to enable equipment to sool to

this temperature.

chief temperature.

Objections were raised to the proposed paragraph 4.5 on the grounds that it did not indicate how compliance with paragraphs 4.f through 4.4 would be determined, that the term "simulated now conditions" was not clearly defined, and that it did not define the vibration to be applied. We do not agree that the ultration need be definied, for example, as one commentator suggested. Bowston need be definied, for example, as one commentator suggested. Bowston need be agree that some classification is meassagy. Accordingly, paragraph 4.8 has been unended to require independent vibration and flow endurance tests of definite duration. The tables have for the commentation in the proposal. been deleted and the requirements now been deleted and the requirements now stated in text form to make it clear that compliance with paragraphs 4.1 through any requirement believed impossible to 4.4 must be shown after the vibration meet. We consider, therefore, that the and flow endurance tests: We agree standards are appropriate minimum refurther that mask-mounted regulator vibration regulator way be less strict than for panel-mounted regulators, and the mask-mounted regulators have been exempted from the vibration requirements. The reference to "demand requirements. The institution of "demand requirements of paragraphs 4.8 and 4.9 is sufficiently clear without listing all specific types in wiew of paragraph 2, Claraffication.

Paragraph 4.10 proposed compliance with paragraph 4.1 although its supplicability extended only to subparagraph

has these veworthed to refer to makimum environmental (dabin) situatie.

The Asidaly rejects the suggestion that "blich let" his used in parsignish 6.2 be carefully defined. As discussed previously in connection with crewmembers middle, 2008; 15; that uses the selection to

quality control, is dependent on a numer of variables so that it is not practical to define it in the TSO. The general requirements of a quality control system are stated in paragraphs 37.5 and 37.15 of the PARs and need not be repeated in the TSO itself. Neither does the Agency agree with a suggestion that would delete the requirement to requalify one regulator for each lot. Requalification provides a check of continued compliance with all the pertinent requirements and is considered essential.

Complying with several responses to the notice, paragraph 7 has been amended to correct the abbreviations and defi-nitions relating to "STPD" and "g". 'ATPD" has been added to the list.

One recommendation that asparate standards be promulgated for maskmounted and panel-mounted regulators has been effectively accomplished by including separate reference, when nec-The TSO, as revised, is therefore applicable to both. Other recommendations that the TSO incorporate installation and operational requirements must be rejected as beyond the general scope and intent of any TSO. A flat recom-mendation that the TSO requirement be equivalent to existing military re-

Furthermore, no comment pointed out any specific unreasonable requirement or any requirement believed impossible to meet. We consider, therefore, that the quirements and do not exceed the stateof-the-art.

Interested persons have been afforded the opportunity to participate in the making of this amendment and all relevant material submitted has been fully considered.

(Secs. \$18(a), 601, Pederal Aviation Act of 1958; 40 U.S.C. 1854, 1421)

In consideration of the foregoing, and pursuant to the authority delegated to capility extended only to subparagraph
411s... The Agency agrees with the commentators who pointed out the Insulations is amended by adding new and paragraph. It has been substitute.

For the reasons discussed previously in connection with TSO-G78, Crewmember personned Obygen Masks, paragraph 5.0 has been verroried to refer the majority majority.

Director, Flight Standards Service.

§ 37.184 Crewmember demand exygen masks—TSO-C78. (a) Applicability. This TSO pre-

scribes the minimum performance standards that aircraft crewmember demand oxygen masks must meet in order to be identified with the applicable TSO marking. New models of demand exygen masks that are to be so identified and that are manufactured on or after February 10, 1967, must meet the require-ments of the following "Pederal Aviation Agency Standard, Crewmember Demand Oxygen Masks."

(b) Merking. Each oxygen man manufactured in accordance with the provisions of this section must be

To indicate whether it is a "non-pressure demand" or a "pressure de-mand" mask;

(2) To indicate the maximum environmental (cabin) altitude for which it is qualified; and

(3) As specified in § 37.7, except that the markings need not include the serial number, the weight, or the date of manmacture.

(c) Data requirements. In accordance with § 37.5, the manufacturer must furnish to the Chief, Engineering and Manufacturing Branch, Flight Standards Division, Pederal Aviation Agency, in the region in which the manufacturer is lo-

cated, the following technical data:

(1) Seven sets of manufacturer's operating instructions and equipment lim-

Itations.

- (2) Seven sets of installation procedures with applicable drawings and specifications, limitations, restrictions, and other conditions pertinent to instal-lation.
- (3) One copy of the manufacturer's est report.
- (4) One copy of the manufacturer's maintenance instructions, inclucionaning and sterilizing procedures. instructions, including
- (d) Previously approved equipment. Crewmember demand oxygen masks approved prior to February 10, 1967, may continue to be manufactured under the provisions of the original approval.

## PEDERAL AVIATION AGENCY STANDARD CREWMEMBER SEMAND CETGEN MARKS

1.0 Purpose. This Standard contains minimum performance standards for the manufacture of demand type oxygen masks for use with nonpressure demand (straight-demand and diluter-demand) and pressure-

demand oxygen systems.

2.0 Design and construction of mask. To be eligible for approval under a Technical Standard Order authorization, the caygen mask must possess the following design and

construction characteristics.

2.1 Masks designed for use with a re-motely located oxygen flow regulator must include a Sexible oxygen supply tube fixed or detachable at the mask or at the regulator or at both. Oxygen supply tubes used in conjunction with mask-mounted exygen flow regulators are not subject to this para-

graph.

3.3 The mask must be designed for res-3.3 The mast must be designed for re-paration through the nose and mouth (oro-mass). The mask may also include inte-gral goggles designed to protect the eyes from smoke and harmful gases (fullface). 2.3 The mask must be constructed of materials that—

(a) Do not contaminate air or oxygen;
 (b) Are not adversely affected by continu-

(c) Are at least flame resistant.

8.4 The mask must be designed to prevent the accumulation of hazardous quantities of expiratory gases within the facepiece chamber.

The mask must be designed to prevent the formation or accumulation of frost which would interfere with the function of the exhalation valve, unless it can be shown that the frost can be removed by external manipulation without removing the mask from the face of the user.

2.6 The fullface mask must be designed to include means for the prevention or the removal of condensation from the inside sur-

faces of the goggle lenses.
2.7 Masks equipped with oxygen supply tubes designed for quick disconnection at the mask or at the regulator must incorpo-rate means to alert the user when his eargen supply tube has become disconnected. Buch must not restrict the flow of ambient air through the oxygen supply tube by an amount exceeding 25 percent. This section does not apply if the quick disconnect de-vice incorporates means to prevent inad-00 by an

vertent separation. 2.0 Performance. Pive masks of each kind for which approval is sought must be abown to comply with the minimum per-formance standards set forth in paragraphs 3.1 through 8.12, except that only one mask of each kind is required to comply with the provisions of paragraphs 3.6, 3.8, 3.9, and 3.11. Tests must be conducted at ambient atmospheric conditions of approximately 50" bg. and 70" F., except as otherwise speci-Sed. One flow rates and pressures must be persected to STPD.

3.1 Quick-disconnect coupling.

force required to separate quick-disconnect couplings not designed to prevent inad-vertent separation must not be less than 10 pounds exerted along the axis of symmetry of

the oxygen supply tube.

2.2 Strength. (a) The mask must be expeble of sustaining a pull force on the suspension device attachment fittings of not less than 35 pounds in any direction for a period of not less than 3 seconds.

(b) The oxygen supply tube assembly must be capable of sustaining a pull force of not less than 30 pounds exerted along the axis of symmetry of the tube for a period of not less than 3 seconds.

(c) The oxygen supply tube assembly must be capable of sustaining an internal pres-

sure of 1.5 p.s.i.g.

8.3 Leakege. (a) The total inward leakage rate, with the complete mask positioned
on the face or on a suitable test stand in a manner which simulates normal use, must not exceed 0.10 LPM, STPD, at any negative differential pressure within the range of from ro to 6.0 inches of water.

(b) Inhalation valves installed in pres-are-demand masks must not backleak more than 0.015 LPM STFD, when subjected to a suction pressure differential of 0.1" E<sub>i</sub>O and not more than 0.15 LPM, STFD, when sub-jected to a suction pressure differential of 12.0" H,O.

(c) The oxygen supply tube assembly must not leak when subjected to an internal pres-sure of 1.5 p.s.i.g. 2.4 Flow resistance. (a) The inspira-

tory resistance of the mask and oxygen suptory reasonance or the many and crypen supply two including the crypen supply connector when inserted in an appropriate mating fitting must not exceed the following negative differential pressures at the corresponding crypen flow rates:

Differential pressure (inches H <sub>2</sub> O)	Flow rate
(inches H <sub>i</sub> O)	(LPM)
0.6	90
1.5	90
2.5	

(b) The expiratory resistance of the mask must not exceed the following positive dif-ferential pressures at the corresponding oxygen flow rates:

Differential pressure (inches H <sub>1</sub> O)		Flow rate (LPM)
1.0		
30		70
8.0	******	100

an Pressure-demand exhalation valve performance. The exhalation valve installed in a pressure-demand mask must see the pressure-demand in a pressure-demand mask must open when the pressure within the facepiece is 30 mm. Hg. and the pressure in the supply tube is 15 to 10.9 mm. Hg.

Vibration. The flow of gases during the respiratory process must not cause vibra-tion, Sutter, or chatter which would interfere with the satisfactory operation of the

fere with the satisfactory operation of the mask.

8.7 Acceleration lead. The exhalation valve must not inadvertently operate under a 5g, load applied in any direction.

8.8 Extreme temperature. The mask must comply with puregraphs 8.3 through 9.5 in an ambient temperature of 70° P. within 15 minutes after being stored at a temperature of 160° P. for 13 hours, and within 15 minutes after being stored at 0° P. for 3 hours. The relative humshity during stored must vary from 8 to 96 percent. The mask facepiece must not be gummy or sticky and must provide a normal seal after the high temperature exposure.

8.9 Low temperature test delay. (a) The mask must function properly, without apparent delay, at a temperature of 70° P. after being stored at a temperature of 20° P. for not less than 3 hours.

(b) The mask must function properly, without apparent delay, and continue for a period of not less than 15 minutes when tested at a temperature of 20° P. after being stored at a temperature of 70° P. for not less than 12 hours.

8.10 Decompression. (a) A mask not equipped with a pressure railef water more

8.10 Decompression. (a) A mask not equipped with a pressure relief valve must not suffer damage and must comply with paragraphs 8.5 through 8.5 after being subparagraphs 3.3 through 3.5 after being subjected to a decrease in ambient pressure from 13 pails, to not less than 2.7 pails, for a straight or diluter-demand kind, or to not less than 2.1 pails, for a pressure-demand kind, within a period of not more than 1 second. This decompression test must simulate the condition that would be imposed on a mask being worn by a crewmember during the specified decompression.

(b) A mask squipped with a pressure relief valve must be subjected to the decompression specified in subjected to the decompression specified the subjected to the decompression specified in subjected to the decompression specified the subjected to the subjected to the subjected to the subjected to the decompression specified the subjected to th

section during which the pressure relief valvenus open at a differential pressure of 17 H.O and must relieve the differential pressure to a value not exceeding 16" H.O within 5 seconds. During the 5-e and interval, the Fure differential must not exce

of 30" H<sub>2</sub>O. The pressure relief value must close at a differential pressure of 14" H<sub>2</sub>O. 3.11 Opening. The mask must comply with paragraphs 3.3 through 3.5 after being subjected to the following simulated breath-ing schedule for a total of \$0,000 cycles:

, Respiratory system	Minute flow rate LPM, STPD	Velume, tidal litera
21, 600 21, 600 4, 600	<b>3</b>	1.0 1.5 2.0

A constant time interval must be maintained

between respiratory cycles.

3.13 Microphone. If the mask is designed to include a microphone, the installation of the microphone must not interfere with the operation of the mask.

4.0 Quality control—4.1 Production tests. Each mask must be shown to comply with the provisions of paragraph 3.3(a), total leakage.

4.2 Rendom tests. One mask must be selected at random from each lot and must be shown to comply with paragraphs 2.1 through 3.12. The lot size must be selected by the applicant subject to the approval of the Federal Aviation Agency (see FAR § 37.5). on the basis of evaluation of the applicant's quality control systems (see § 37.5(a) (3)). 5.0 Maximum environmental (sebin) of-

titude. The minimum pressure to which the mask has been shown to decompress satisfactured to the control of the (a) or (b) of this standard determines the maximum environmental altitude of the maximum environmental altitude of the mask, except that it shall not exceed the value shown in the following table:

	ntel (cebin)		
	altitude	Eind o	
000,00	Stot	Straight i	er Diluter
		·· Demand	
45,000	fort	Pressure I	lemand.

6.0 Abbreviations and definitions.

LPM: Liters per minute. STPD: Standard temper

dry (0° C. 700 mm. Hg.).

usy (u\* U. Teo Min. Hg.).
p.s.ig.: Pounds per square inch, gage.
p.s.ia.: Pounds per square inch, absolute.
g.: Acceleration of gravity, 23.2 fost/second.\*
Tidal volume: Volume of air inspired per breath.

## .198 Oxygen regulators, demand-TSO-C89. 4 37.196

(a) Applicability. This technical standard order prescribes the minimum performance standards that aircraft demand oxygen regulators must meet in order to be identified with the applicable TBO marking. New models of de-mand oxygen regulators that are to be so identified and that are manufactured on or after Pebruary 10, 1967, must meet the requirements of the following "Federal Aviation Agency Standard, Oxygen Regulators, Demand."

(b) Marking. In addition to the markings required by § 37.7, the inlet supply pressure range and the maximum environmental (cabin) altitude must also

be marked on the regulator.

(c) Data requirements. The manufacturer must furnish the Chief, Engineering and Manufacturing Branch, Flight Standards Division, Pederal Aviation Agency, in the region in which the manufacturer is located, the following technical data:

(1) Seven copies of the manufacturer's operating instructions, equipment limitations, and installation procedures.

(2) One copy of the manufacturer's

(d) Previously approved equipment. Oxygen regulators approved prior to Pebruary 10, 1967, may continue to be manufactured under the provisions of the original approval.

## PRINCIAL AVIATION ASSISTS STANDARD

OXYGEN RESULATORS, REMAINS

- 1. Purpose. This standard contains minimum performance and quality control standards for the manufacture of demand orygen system regulators.
- 2. Classification. The term "demand regwheter includes all of the following classes of regulators:
- (a) Straight demand regulators designed to deliver oxygen enly.

(b) Diluter demand regulators designed to deliver a mixture of oxygen and air, and CEYPER ORLY.

(c) Straight demand pressure breathing regulators (straight demand regulators designed to deliver undiluted oxygen under

signed to deliver demand pressure breathing regulators (diluter demand regulators de-aigned to deliver undiluted oxygen under

agence to survey tensitated oxygen tensor positive pressure).

3. Design and construction of regulator. To be eligible for approval under a TSO authorization, the regulator must possess the following design and construction characteristics.

9.1 Demand regulators designed to be mounted directly upon an exygen mask or the crowmember's clothing or safety harness must include a Serible exygen supply tube connecting the regulator inlet with the exy-

gen supply system.

8.2 Demand regulators must be constructed of materials that—

(a) Do not contaminate air or oxygen; (b) Are not adversely affected by continu-ous contact with exygen; and (c) Are at least flame resistant.

equipped with a 200-mesh screen, or equiv-

squipped with a sub-main screen, or equiv-elent filter, at the oxygen inlet port or at the oxygen inlet hose assembly. (b) Diluter demand and diluter-demand pressure regulators must be equipped with acreening of not more than 100 mesh and not than 30 mesh, or equivalent filter, at the

air inlet port. 3.4 Diluter demand and diluter-demand pressure breathing regulators must be pro-vided with a means for manually selecting a delivery of undiluted oxygen. If the selection means is controlled by a rotating handle or lever, the travel must be limited to not more than 180 degrees from the "normal oxygen" position to the "100 percent exygen" position. The dilution position of the selection means must be designated "normal lection means must be designated "normal oxygen" and the nondilution position must be designated "100 percent oxygen." The selection means must be such that it will not assume a position between the "normal oxygen" and "100 percent oxygen" positions.

3.5 Straight demand pressure breathing and diluter demand pressure breathing regulators must be designed to provide oxygen at a nositive pressure of 11 0.230 inches H O

at a positive pressure of 11.0±3.0 inches H.O to determine mask peripheral leakage at altitudes below which positive pressure are hereinafter required. The means of obtaining this pressure must be by push, pull, or toggle control appropriately marked to indi-

cate its purpose

3.6 Diluter demand and diluter demand 3.6 Diluter demand and diluter demand pressure breathing regulators must incorporate means to indicate when oxygen is and is not flowing from the regulator outlet. This requirement does not apply to mask

mounted regulators.

4. Performance. Two demand regulators of each class for which approval is sought must be shown to comply with the minimum must be anow to company with the minimum performance standards set forth in para-graphs 4.1 through 4.10 in any position which the regulators can be mounted. Tests must be conducted at ambient atmospheric conditions of approximately 30 inches Hg and 70° F., except as otherwise specified. It is permissible to correct gas flow rates and pressures to STPD conditions by

4.1 (a) Demand regulators must supply not more than the specified outlet pressures. These characteristics must be displayed at all altitudes, with the oxygen supply pressure at all values within the design inlet pressure range, and with the diluter valve open and eleced.

Plow.	suction p	resente
LPM, ATPD:	inches e	f water
<b>*</b>		<b></b>
7		
160		1.00

(b) Demand regulators must not flow more than 0.01 LPM, STPD, when the cutlet suction pressure is reduced to 0 inch of E,O under the conditions specified in subparagraph (a) of this paragraph.

4.3 (a) Diluter demand and diluter demand pressure breathing regulators must supply the following percentages of sylinder engine, by volume, at the specified atmospheric pressure and corresponding altitudes. These oxygen percentages must be delivered at regulator outlet gas flows of 20, 70, and 100 LPM. ATPD, with the oxygen supply pressure at all values within the design inlet pressure range.

	Altitude	Minimum percent ogygen	
Pressure mm Hg		Diluter	Diluter de- mend pro- sure breathing
760 622. 4 622. 6 620. 1 360. 5 362. 4 224. 1 170. 3	98558888888888888888888888888888888888		a 28 38 44 364

Not applicable.

Not applicable.

(b) Stratgs (Microsoft and an initial Columnate pressure base thing application might supply not less than 68 percent origins, by volume, it all alimitates under the conditions specific in subparagraph (a) of this paragraph (3 (6) individual common pressure breathly ing regulated with the dilutate raise open calcional Mail Invitable desirable principles beauting regulation, must provide positive breathing pressure at a few of 20 LPM, ATPD, in accordance with the foliables as the conditions of t

<b>Aittudt</b> 1.000 feet	Positive outlisf
	*==*===****
40	-0.0 8.6 <b>22.6</b>
4*	.******
****	

(by The positive pressure at 100 LPM, ATPD, must not decrease by mom that 0.8 inch H 0 from the pullure pressure di

0.8 inch H 0 from the pusitive pressure of 20 LPM. AUFD.

(c) The positive pressure at 0.01 LPM. AUFD.

(c) The positive pressure at 0.01 LPM. AUFD.

(d) The positive pressure at 0.01 LPM. AUFD.

0.8 inch E0 from the positive pressure st 20 LPM. ATPD.

4.4 (c) Tableinvand is hagoda strifthresign the resultation at MM iskel must not exceed 0.1 LPM. ETPD, with 8 studden pressitive at 1.0 inch H0 applied to the outlet part, the oxygen supply inlet port scaled, had the distor valve closed.

(b) The outward issuage of air tilrough the resultates at fee level must not exceed 0.1 LPM. STED Sylin M issuirs publicated at inches E0 applied to the outlet port, the express unpull-inishing teelid, and the Citiose valve open and closed.

(c) The regulator outlet leakage must not

(c) The regulator outlet leakage must not seed 0.01 LPM, STPD, with the regulator outlet port open and any oxygen supply esure within the specified operating range

applied at the regulator inlet port.

(d) The regulator overall leakage must not exceed 0.01 LPM, STPD, with the regulator Sow conditions:

cles outlet part scaled and the regulator inlet ure, pressurized to a value equal to the mass presurined to a value of presure specified exygen supply presure.

(a) Granghs demand pre-

(J) (a) Straight demand preserve security and diluter demand preserve breathing quinters must comply with perspected of S arough 44 after a negative pressure of 30 nobes 2,0 and a positive pressure of 54 nobes 2,0 are applied to the outlet part or a period of 2 minutes. The diluter valve

inches E,O are applied to the crelet part for a period of 2 minutes. The diluter valve and the regulator inlet peri must be closed during these two pressure tests.

(b) Straight demand and diluter demand regulators must comply with paragraphs 4.1 through 4.6 after a negative pressure of 20 inches E,O and a positive pressure of 25 inches E,O are applied to the outlet part for a period of 2 minutes. The diluter valve and the regulator inlet part must be closed dur-ing these two pressure tests.

the regulator inlet port must be closed during these two pressure tests.

(c) Demand regulation must camply with paragraphs 4.1 through 4.4 after a positive pressure of 1.5 times the maximum expensively pressure is applied to the inlet port, or to the inlet of the expensively tube in the case of mask measured regulators, for a pariod of 2 minutes. The positive pressure must be applied rapidly to emulate rapid valve must be closed that the outset port must be maded during the test.

valve must be closed and the outset port must be sealed during the test. 4.8 (a) Straight demand and diluter de-mand regulators must comply with para-graphs 4.1 through 4.4 after being subjected to a change in pressure from not less than 18.3 p.a.i.a. to not less than 2.7 p.a.i.a. in not more than 1 second.

(b) Straight demand pressure breathing and diluter demand pressure breathing regulators must comply with paragraphs 4.1 through 4.4 after being subjected to a change in pressure from not less than 13.3 p.s.l.s. to not less than 3.1 p.s.l.s. in not more than

4.7 Demand regulators must comply with paragraphs 4.1 through 4.4 under each condi-tion specified in subparagraphs (a) through (d) of this paragraph with the maximum oxygen supply pressure applied to the regula-tor inlet:

(a) At a temperature of approximately 70° P. after being stored at a temperature of not less than 180° P. for 12 hours.
(b) At a temperature of 70° P. after being stored at a temperature of not warmer than

-67° F. for 2 hours.

(c) At a temperature of not less than 130° F. (d) At a temperature of not more than

4.8 Demand regulators must comply with paragraphs 4.1 through 4.4 after being subjected to the tests specified in subparagraphs (a) and (b) of this paragraph.

(a) The regulator must be vibrated along each mutually perpendicular axis for 1 hour (3 hours total), at a frequency of 8 to 800 ope, and at a double amplitude of 0.036 inches or an acceleration of 2 "g," whichever occurs first. Mask mounted regulators need not be subjected to this vibration test.

(b) The regulator must be subjected to an endurance test of a total of 250,000 breathing cycles. The peak breathing rate must be 30 LPM. STPD. for 200,000 cycles, and 70 LPM. STPD, for 80,000 cycles. The dilution valve must be open during one half of the 50,000 cycles and one cycles cycles and one cycles cycl cycles, and it must be closed during the re-maining cycles. During the nonflow portion of the 30 LPM and 70 LPM breathing cycles. respectively, must be applied to the regulator

Demand regulators must be free of vibration, flutter, or chatter that will prevent compliance with paragraphs 4.1 through 4.3 when subjected to the following simulated

Cycles	Peak Sow per eyels LPM, STPD	Back pressure at 0 LPM, makes H <sub>2</sub> O	Diluter valve
A, 600	100	1.6	Cleard.
A, 600	360	1.6	Open.

4.10 Demand regulators, when subject to accelerations up to 8 "g." in any position, must comply with paragraph 4.1(a) except that the specified suction pressures may be exceeded by not more than 0.6 inches H.O.

5. Maximum environmental (cabin) elti-tude. The minimum pressure to which the regulator has been shown to comply under paragraph 4.6 (a) or (b) of this standard determines the maximum environmental (cabin) altitude of the regulator, except that the maximum environmental (cabin) alti-tude must not exceed the value shown in the following table:

	Chaes	Post
Straight	or diluter-demand	40, 000
Pressure	demand	45, 800

6.3 One regulator selected at random from each lot must be shown to comply with paragraphs 4.1 through 4.10. The lot size may be selected by the applicant subject to the approval of the Pederal Aviation Agency on the basis of evaluation of the quality control system of the applicant (see PAR, § 87.5).

7. Abbrevictions and definitions.

LPM: Liters per minute.

ETFD: Standard temperature and pressure, dry (0° C., 700 mm. Hg., PH.O=0).

ATTD: Ambient temperature and pressure, dry (70° P.; ambient pressure; PH.O=0).

c.p.a.: Oyoles per second.

p.s.i.a.: Pounds per square inch absolute.

g.: Acceleration of gravity, 23 feet/second/second.